

Impedance Control for Robotic Assembly

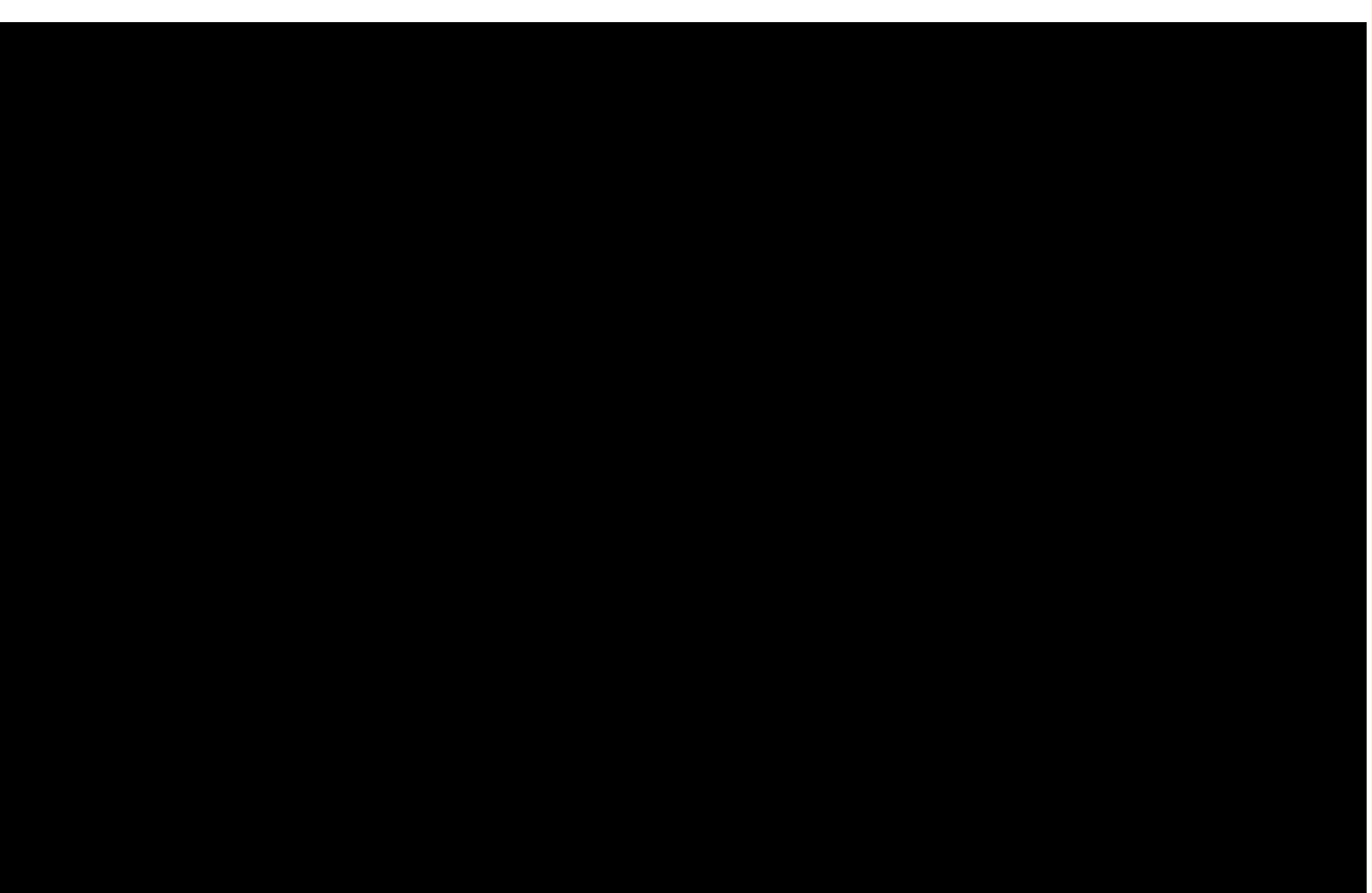
Ron Lumia

University of New Mexico, Albuquerque, USA

Topics

- Swing Free Control
- Laser Tag
- Impedance Control
- Peg and Hole Assembly - jamming/wedging
- Real-time Control to Prevent Jamming and Wedging
- Assembly using Attractive Regions
- DARPA demos
- Conclusions

Swing-Free Trajectory



Laser Tag



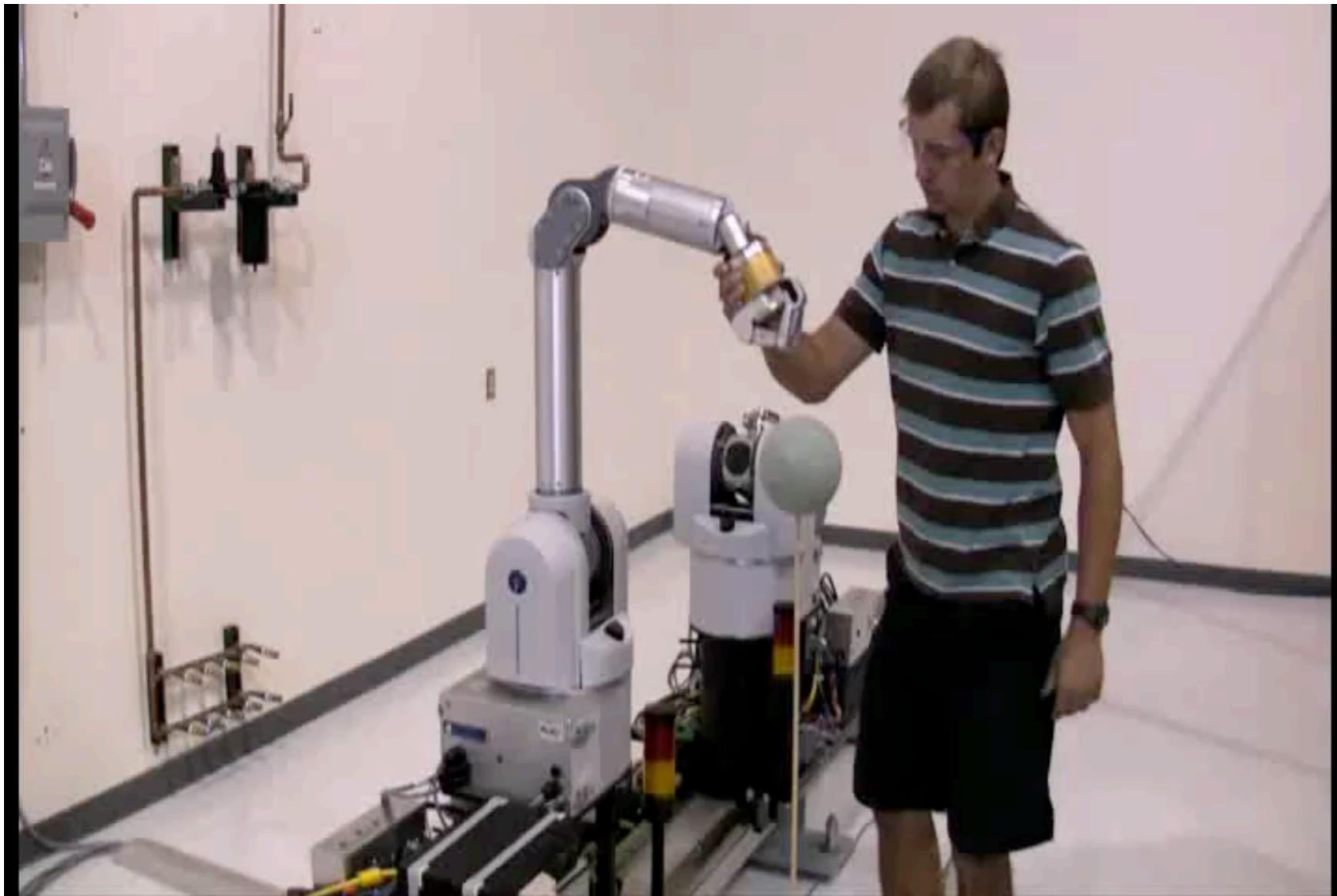
The Lab



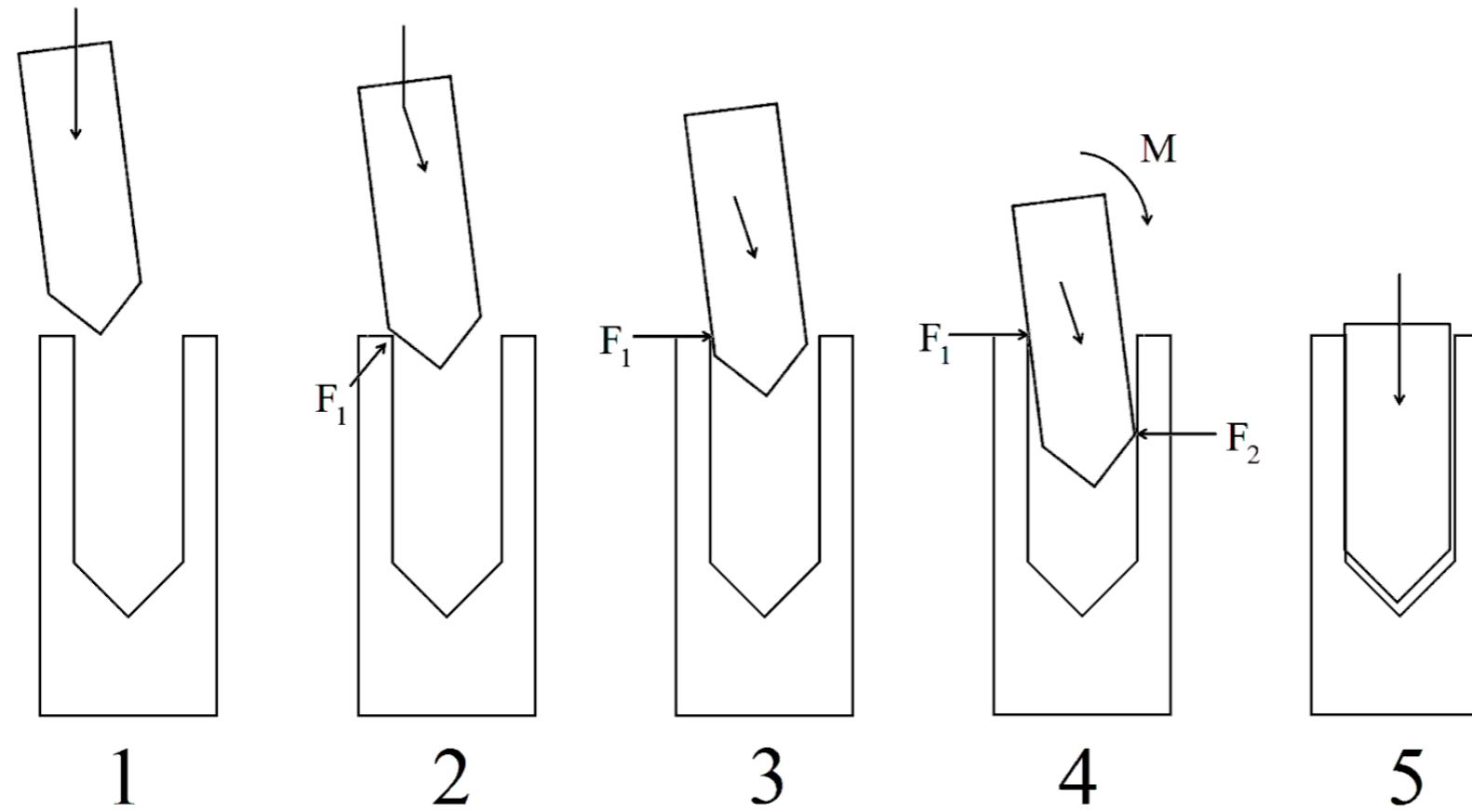
Impedance Control Concept



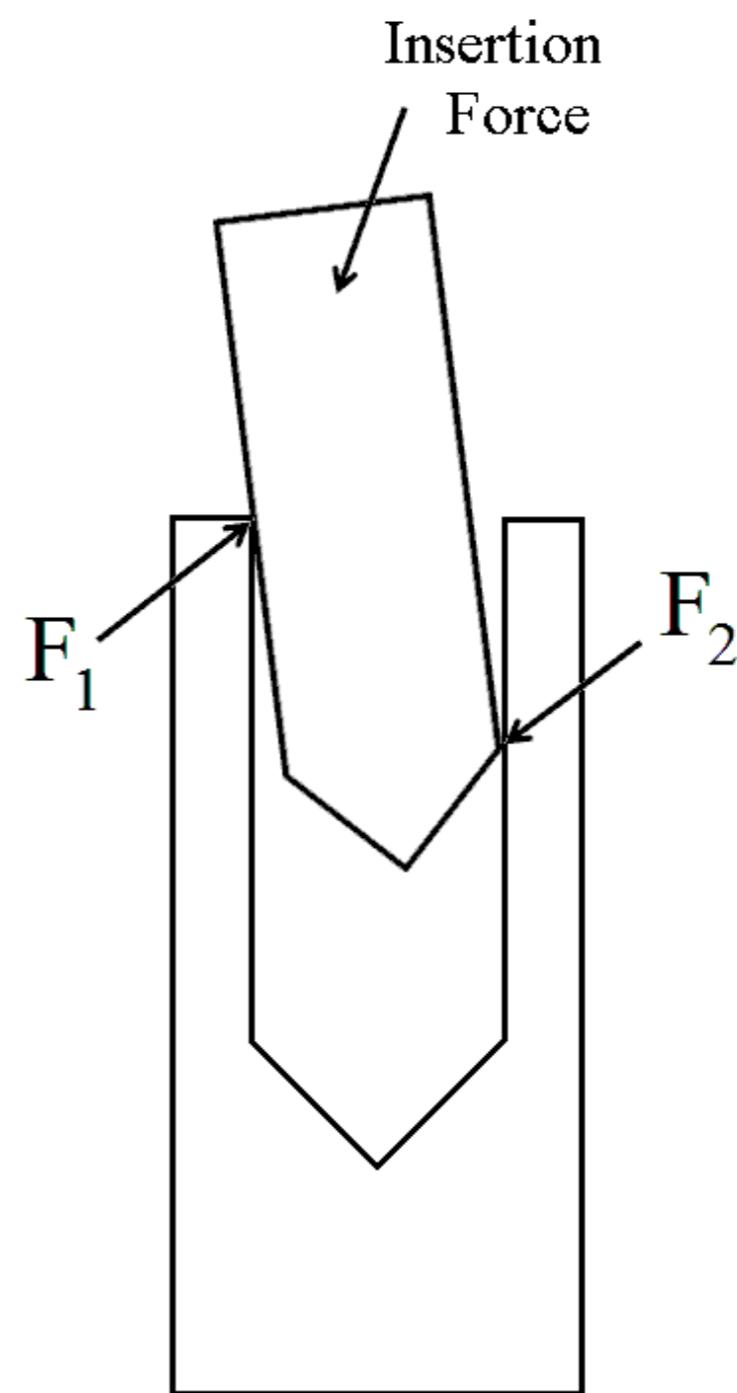
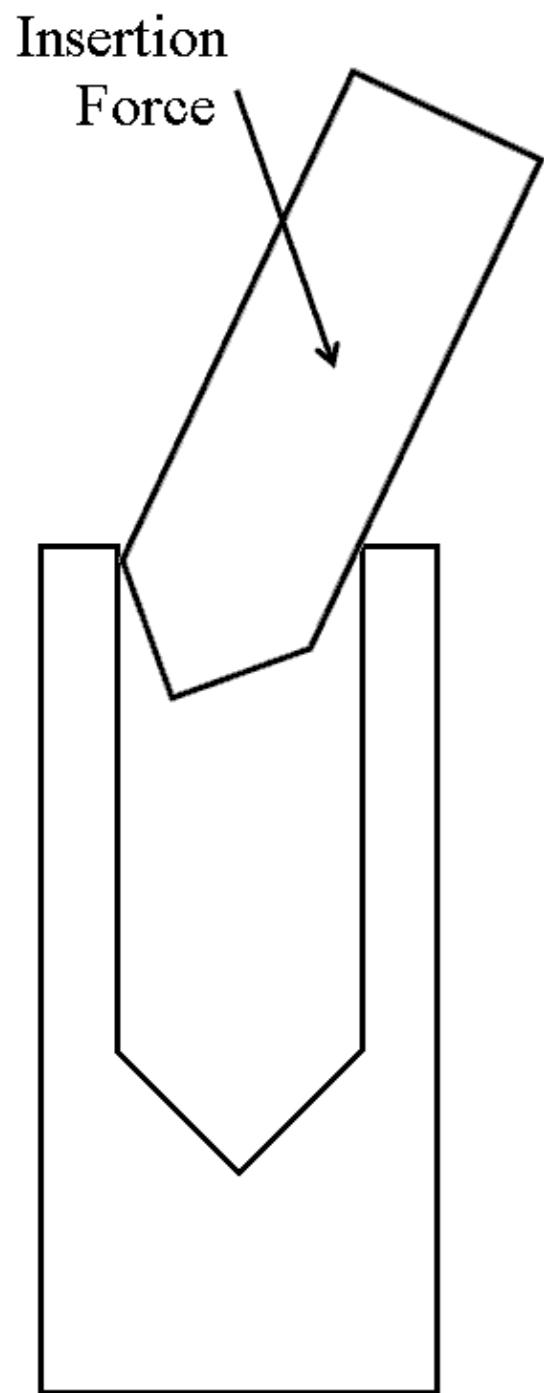
Impedance Control - Sphere Avoidance



Peg in Hole Assembly



Jamming and Wedging



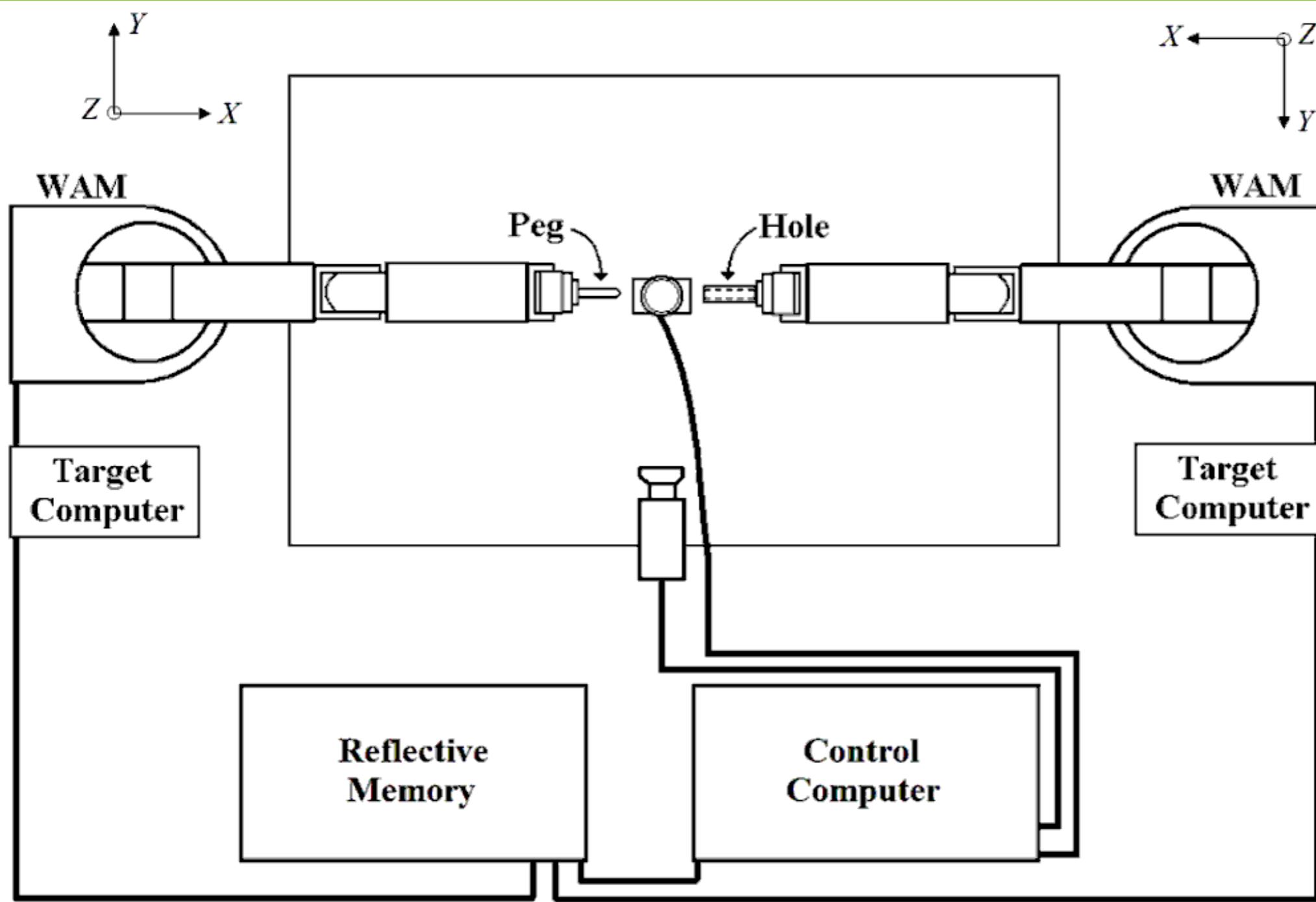
Chamfer Crossing Analysis

$$F_z = \frac{K_x K_\theta (\cos(\pi/2 - \alpha) + \mu \sin(\pi/2 - \alpha)) \left(\frac{z}{\tan(\pi/2 - \alpha)} \right)}{(K_x L^2 + K_\theta) (\sin(\pi/2 - \alpha) - \mu \cos(\pi/2 - \alpha)) - K_x L r (\cos(\pi/2 - \alpha) + \mu \sin(\pi/2 - \alpha))}$$

$$F_x = \frac{-K_x K_\theta \left(\frac{z}{\tan(\pi/2 - \alpha)} \right) (\sin(\pi/2 - \alpha) - \mu \cos(\pi/2 - \alpha))}{(K_x L^2 + K_\theta) (\sin(\pi/2 - \alpha) - \mu \cos(\pi/2 - \alpha)) - K_x L r (\cos(\pi/2 - \alpha) + \mu \sin(\pi/2 - \alpha))}$$

$$M = \frac{K_x L K_\theta \left(\frac{z}{\tan(\pi/2 - \alpha)} \right) (\sin(\pi/2 - \alpha) - \mu \cos(\pi/2 - \alpha))}{(K_x L^2 + K_\theta) (\sin(\pi/2 - \alpha) - \mu \cos(\pi/2 - \alpha)) - K_x L r (\cos(\pi/2 - \alpha) + \mu \sin(\pi/2 - \alpha))} \\ - \frac{K_x K_\theta \left(\frac{z}{\tan(\pi/2 - \alpha)} \right) (L (\sin(\pi/2 - \alpha) - \mu \cos(\pi/2 - \alpha)) - r (\cos(\pi/2 - \alpha) + \mu \sin(\pi/2 - \alpha)))}{(K_x L^2 + K_\theta) (\sin(\pi/2 - \alpha) - \mu \cos(\pi/2 - \alpha)) - K_x L r (\cos(\pi/2 - \alpha) + \mu \sin(\pi/2 - \alpha))}$$

Lab Schematic

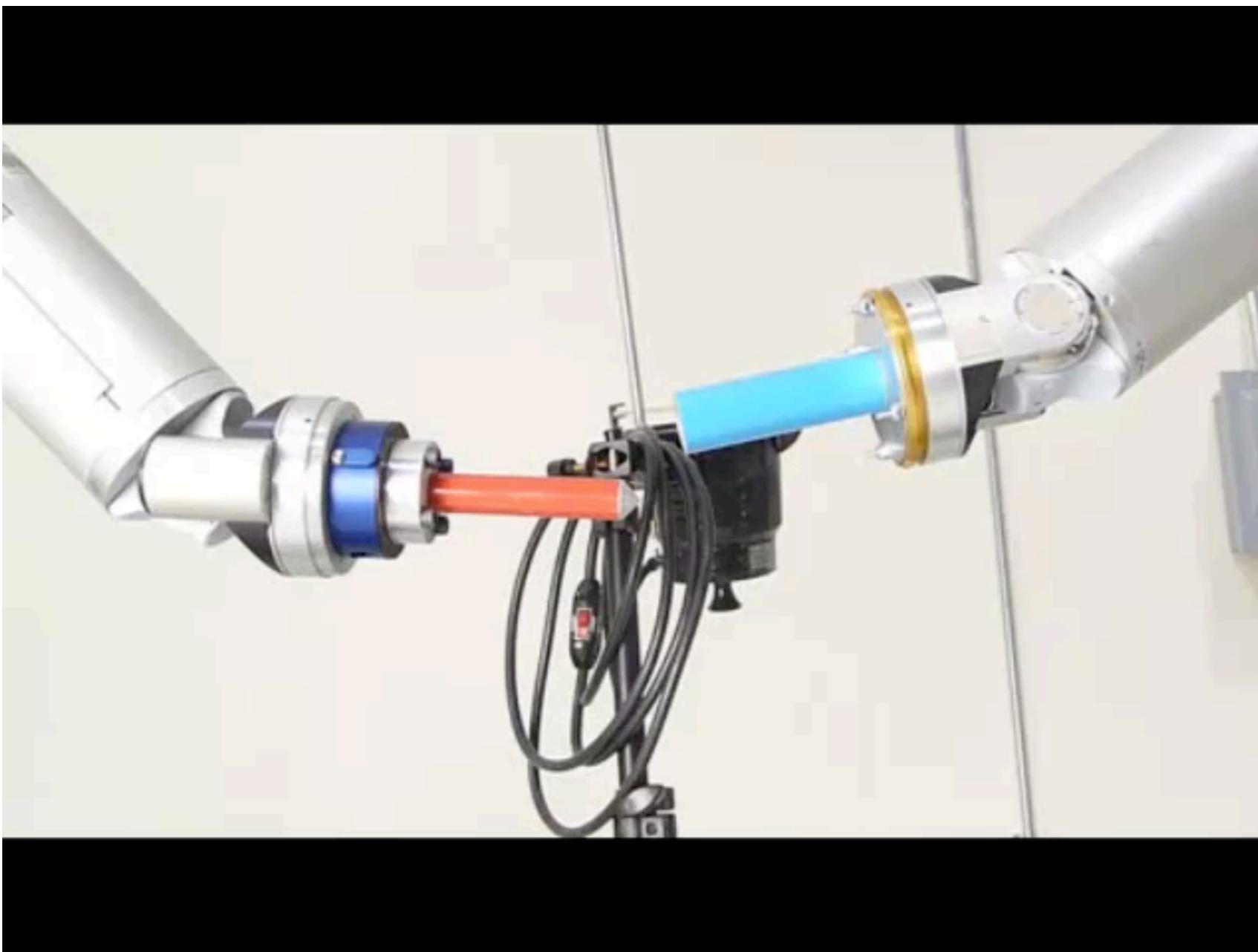


Failure Example

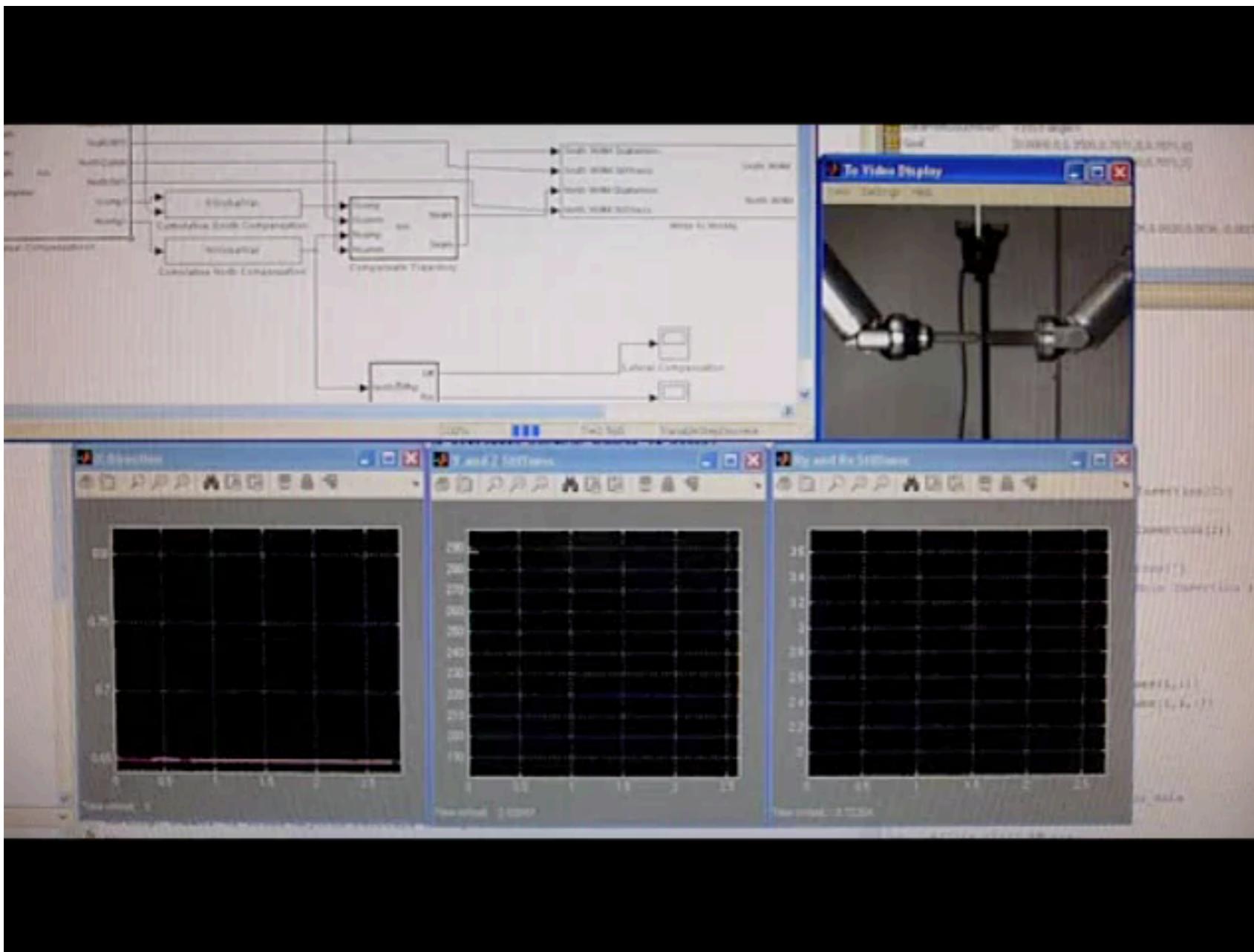
WAM Impedance
Controller for Peg
and Hole Assembly

Virtual RCC Turned OFF

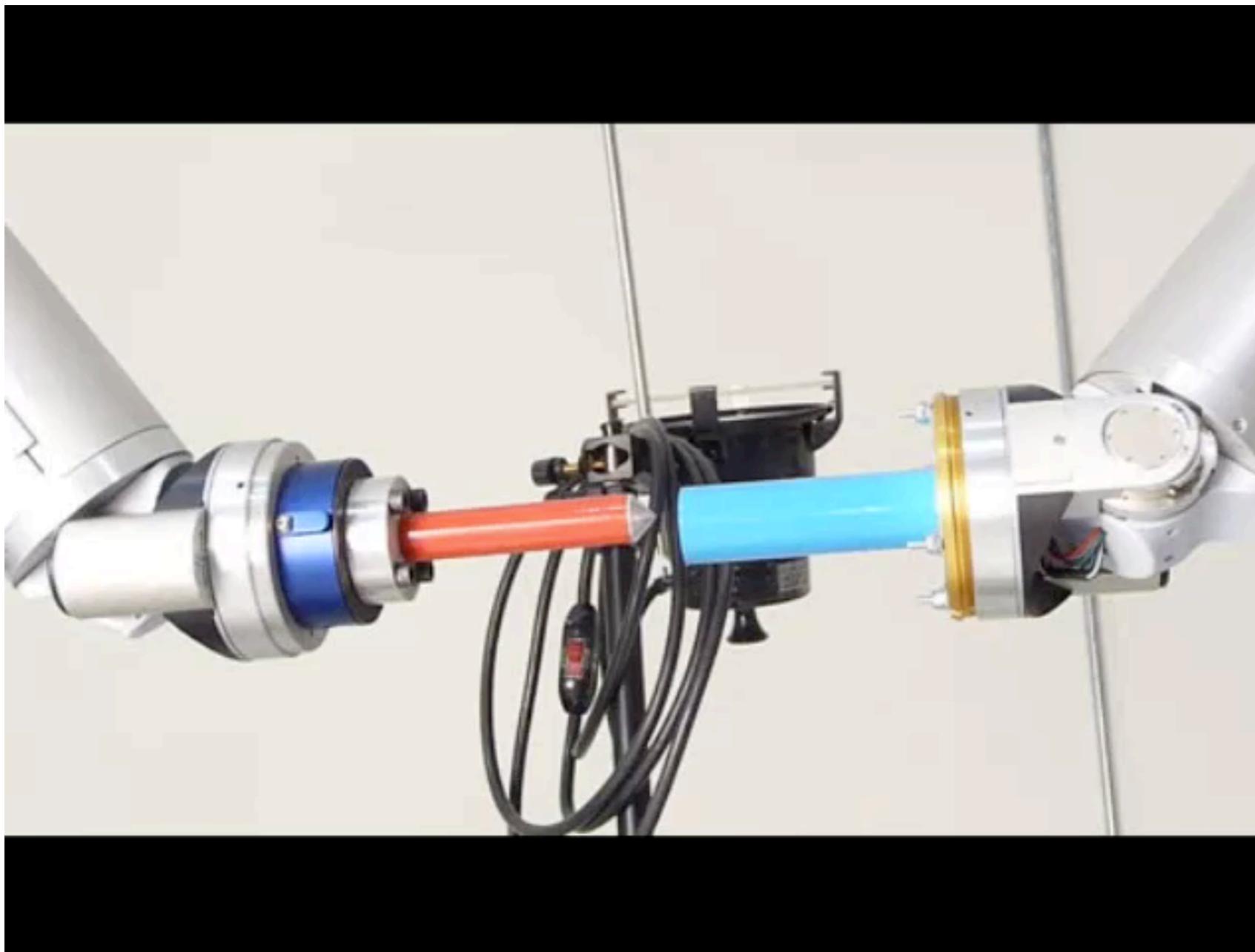
3 Second Insertion



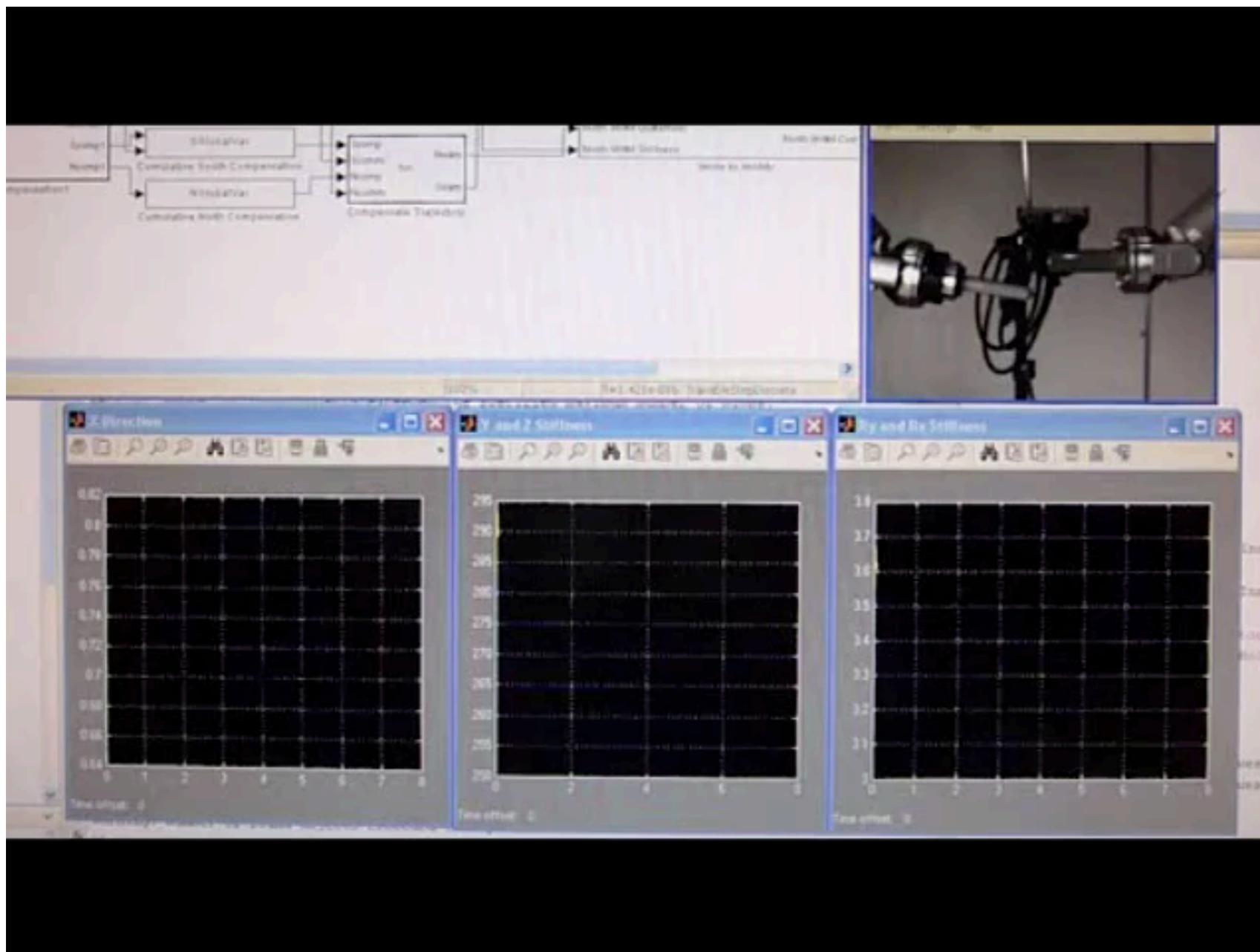
2 Seconds - No Jam



1 Second Insertion



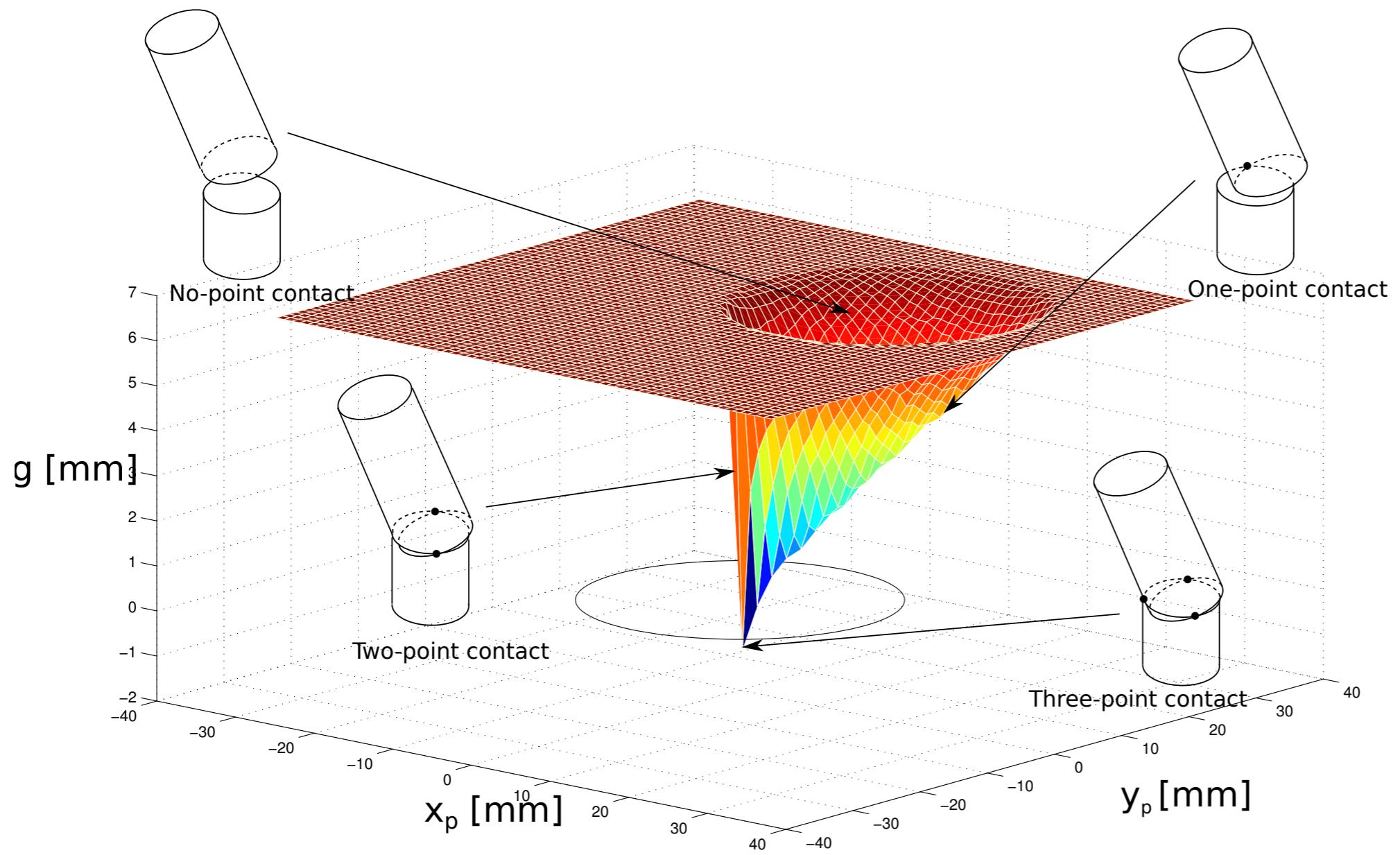
Clear Major Jam



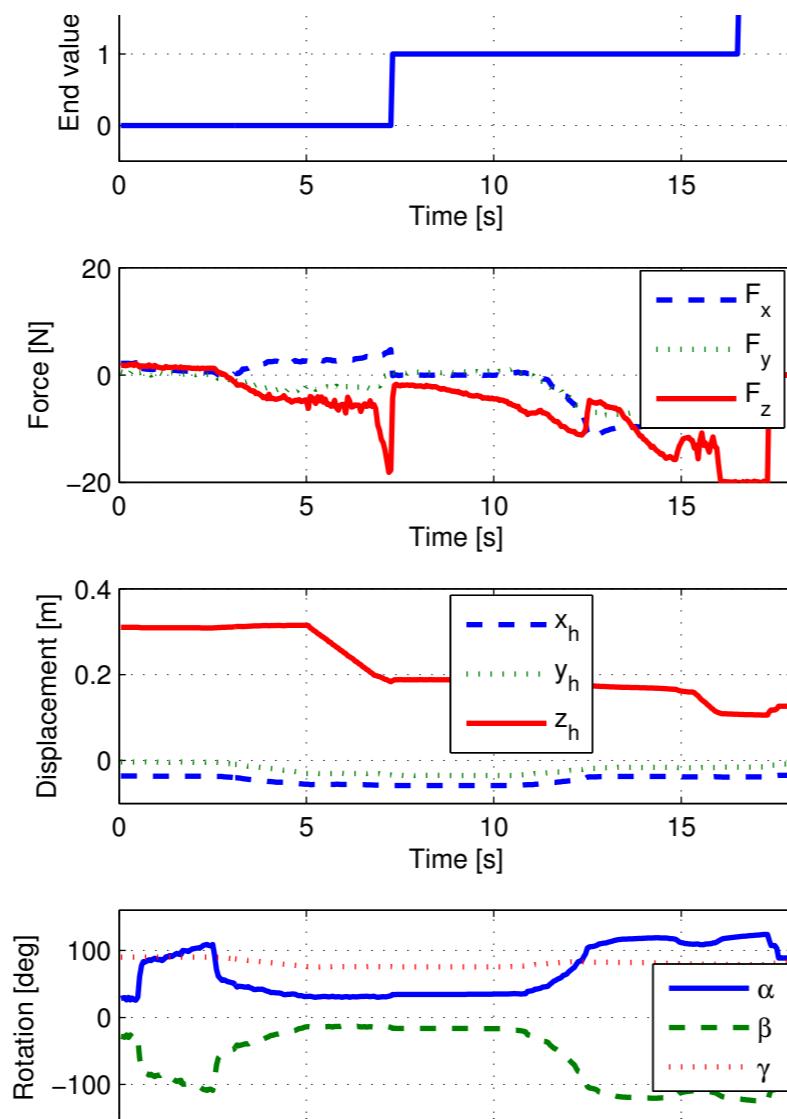
Assembly Planning

- Matteo Gilli, Politecnico di Torino
- Attractive regions + decomposition of 6-D configuration space
- Impedance controller
- Use of “events” rather than time to plan sequence

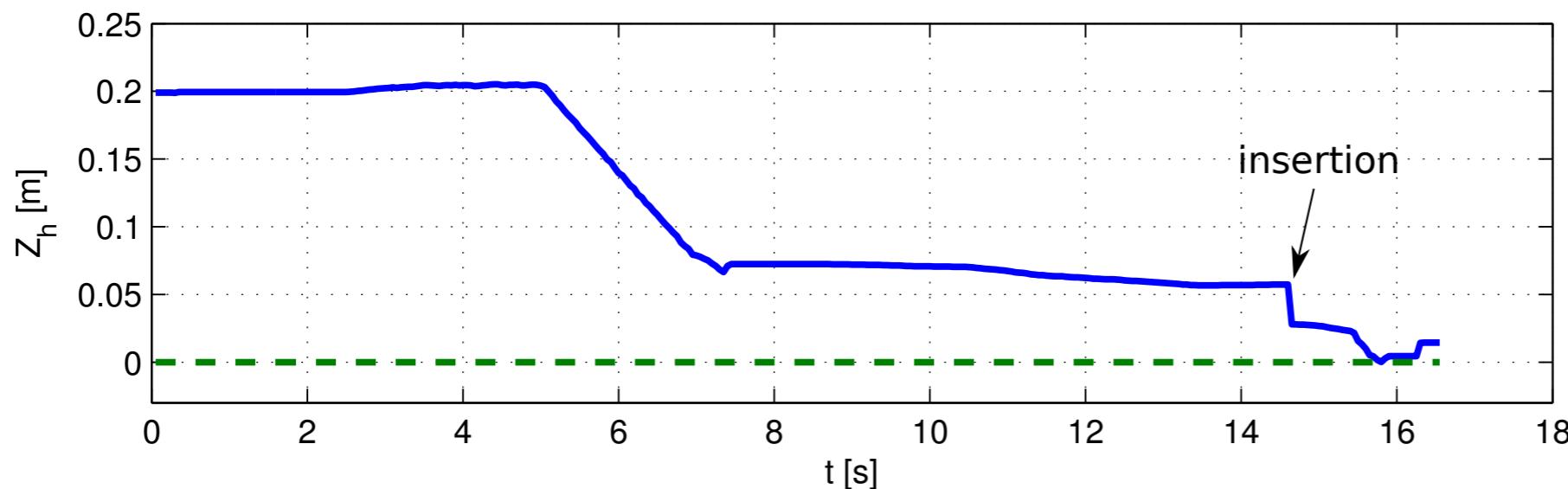
Attractive Region



States not Time



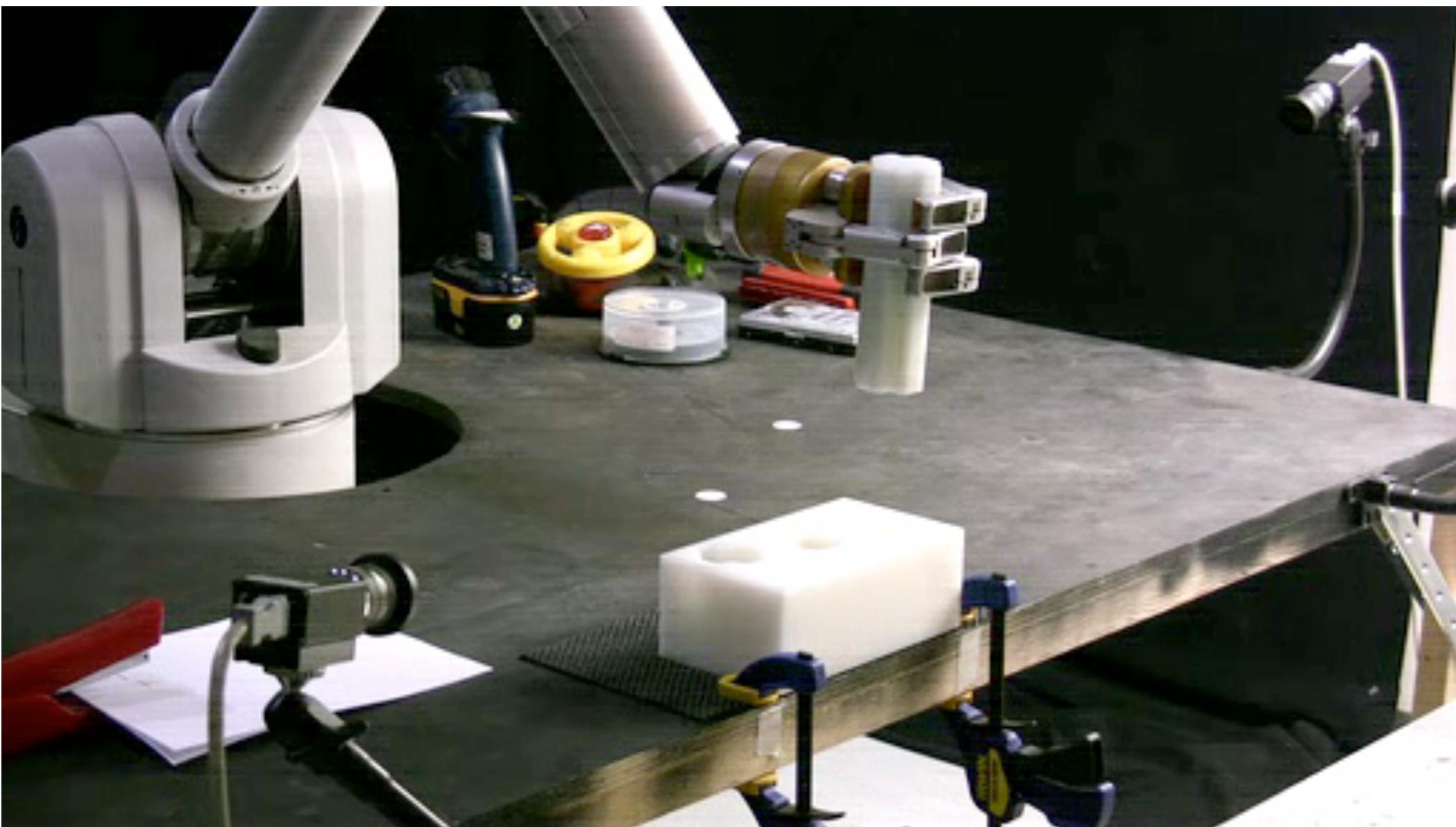
Insertion Progress



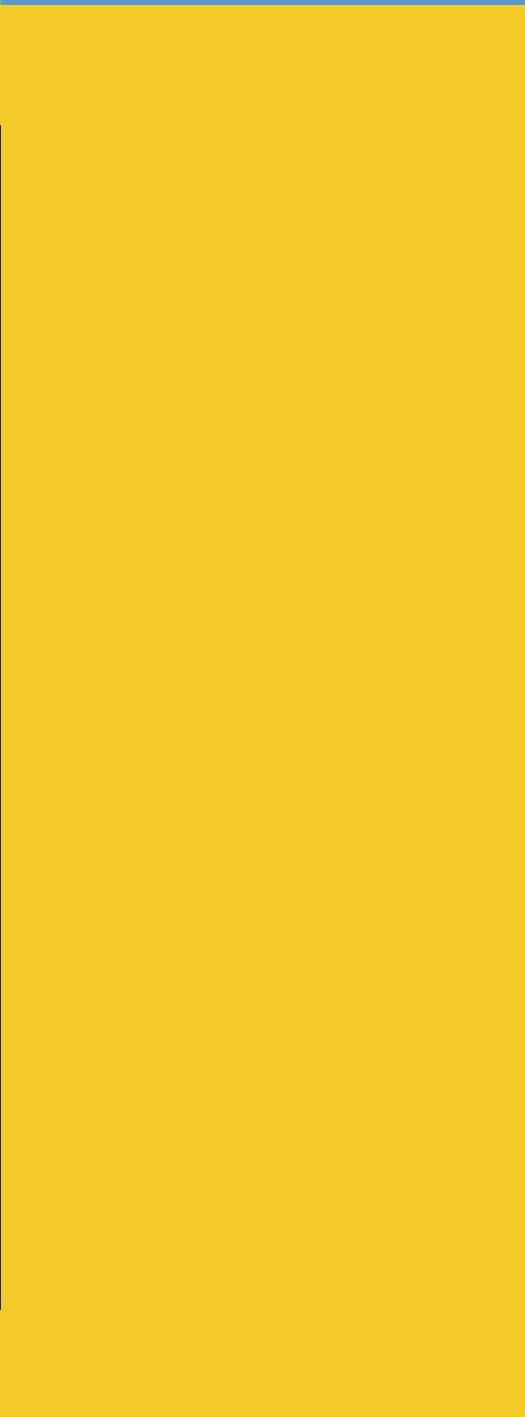
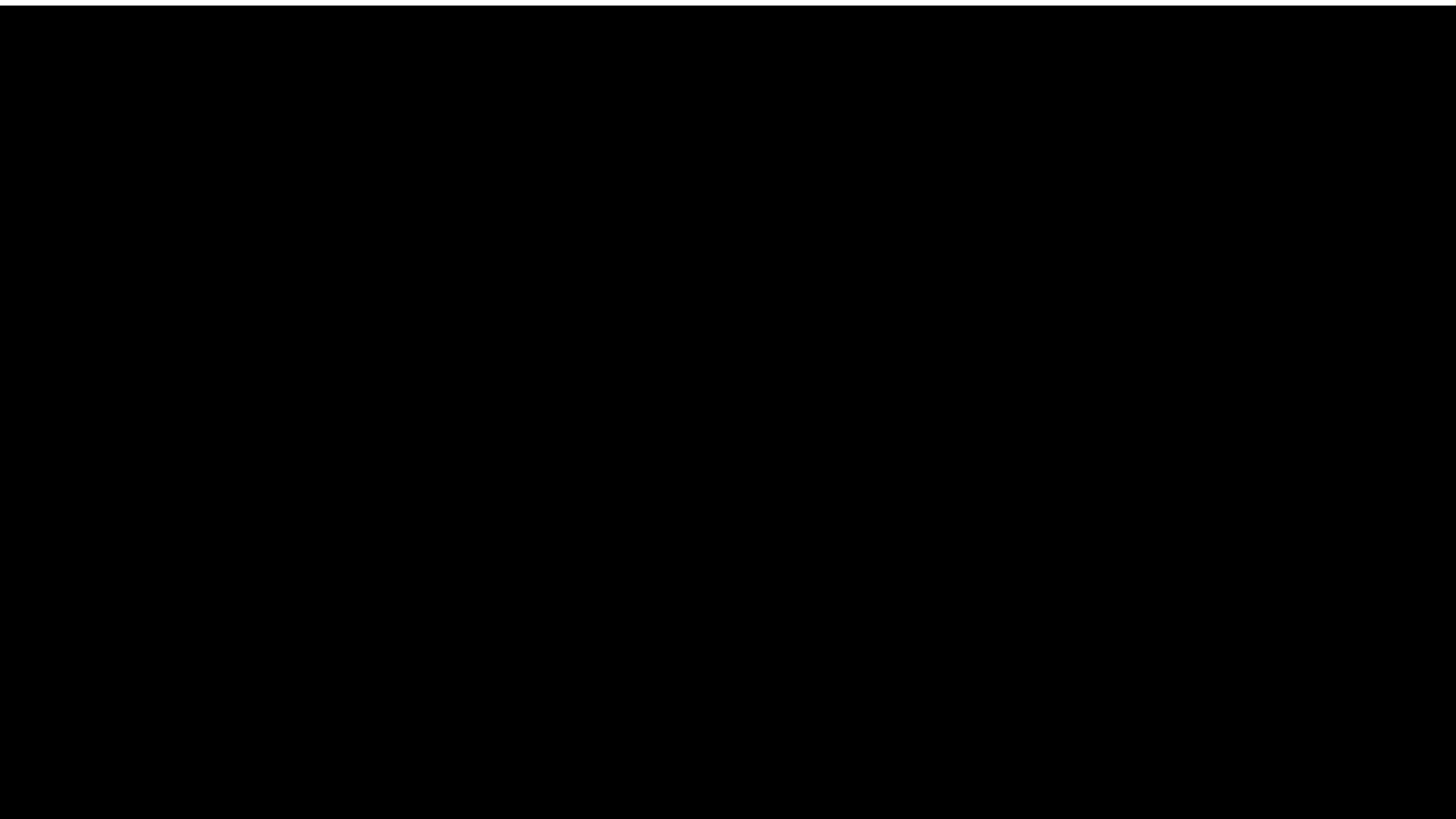
Grasp Peg



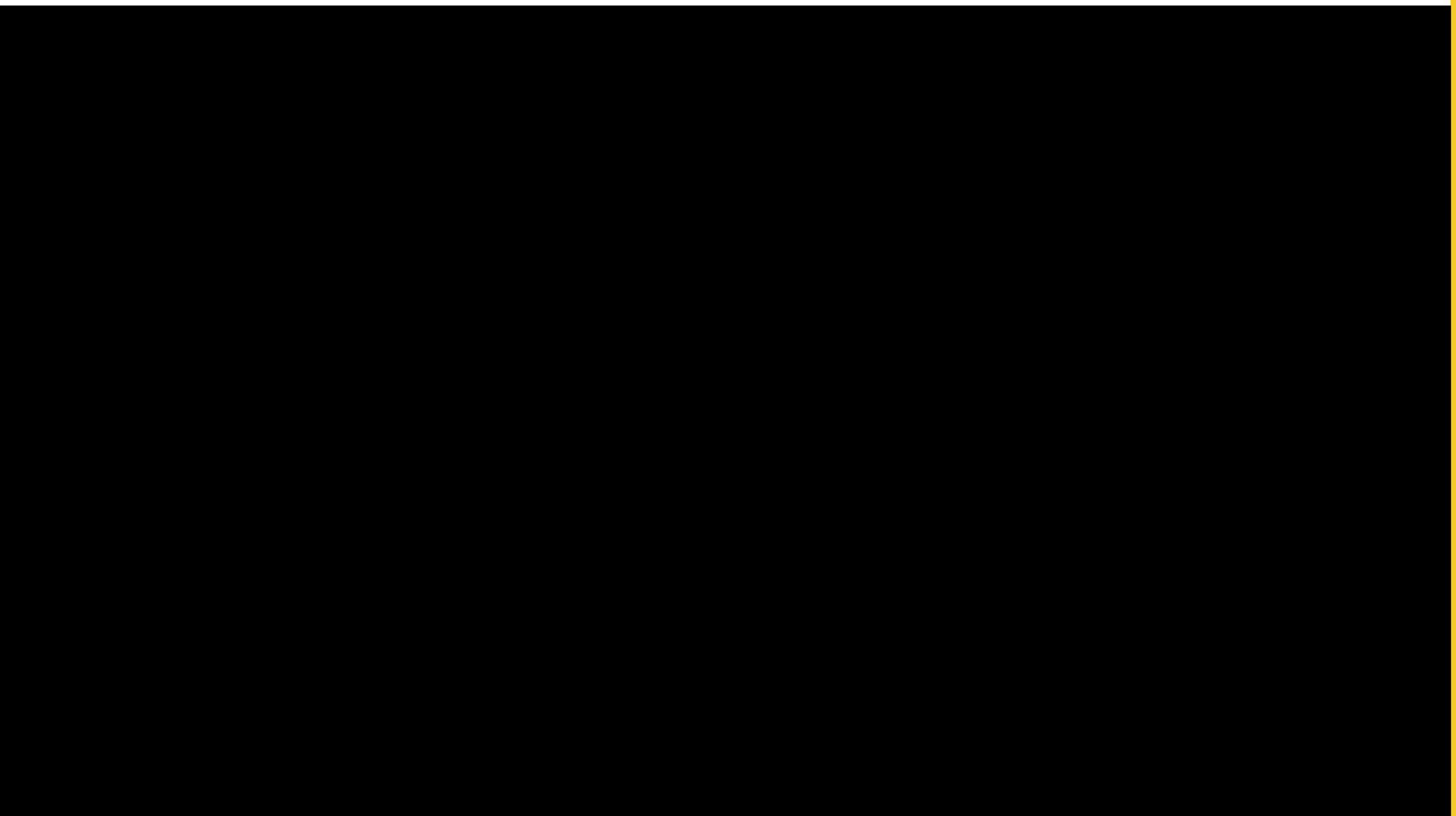
Insert Peg



Staple and Drag



Key Insertion



Open Door



Sponsors

- DOE
 - This work is supported by DOE Grant #DE-FG52-2004NA25590 awarded to the UNM Mfg. Engr. Program. Principal Investigators are John Wood, Ron Lumia, and Greg Starr.
- NSF
 - This material is based upon work supported by the National Science Foundation under Grant No. IIS-0911133, CNS-0549563, and IIS-0329106.

Conclusions

- Non-impedance control algorithms
 - swing-free
 - laser tag
- Impedance control algorithms
 - assembly
 - staple and drag
 - key insertion
 - door opening

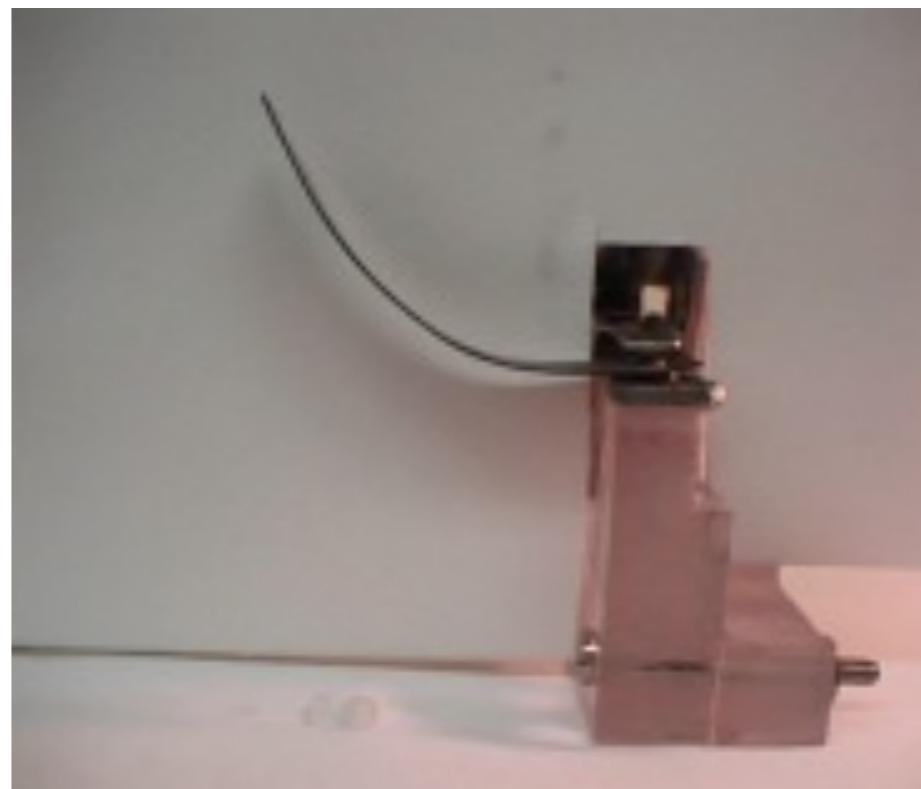
Questions



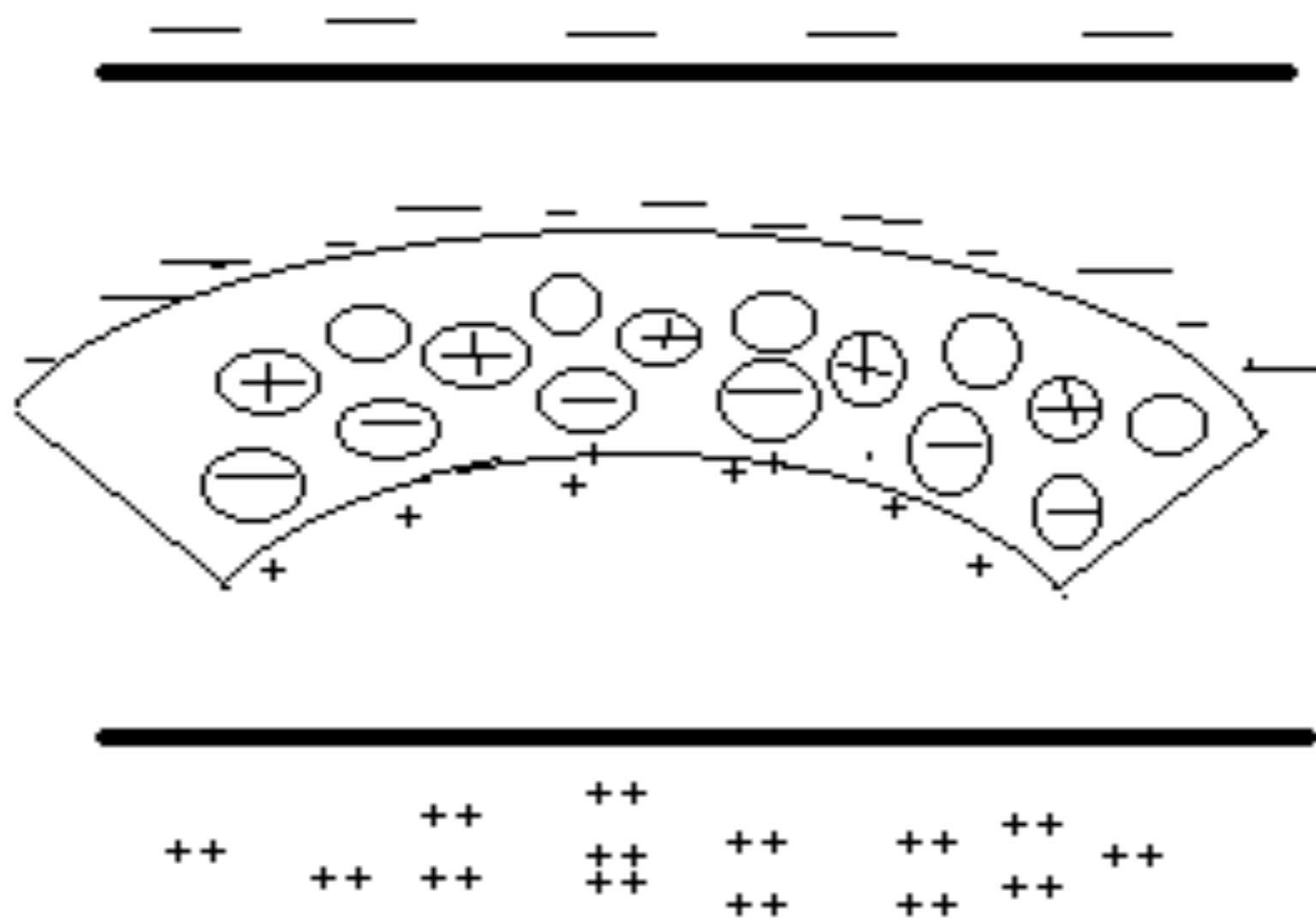
Robotics: Small

- Ionic Polymer Metal Composite (IPMC) microgrippers
- Biological applications, e.g., cell micromanipulation

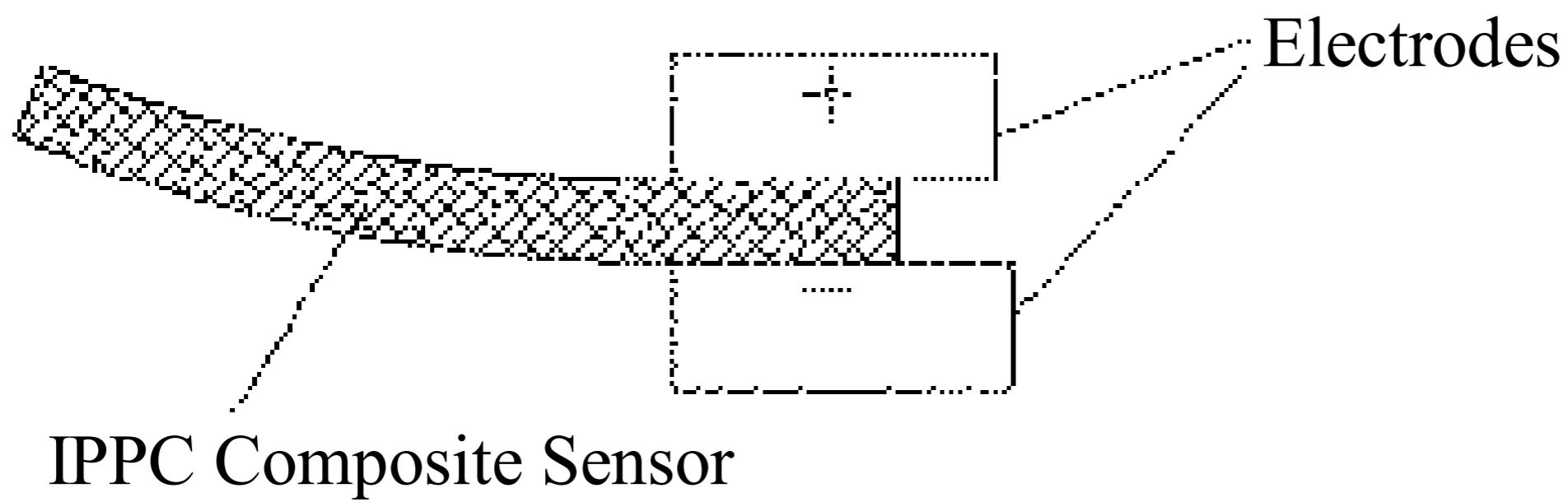
IPMC Microgrippers



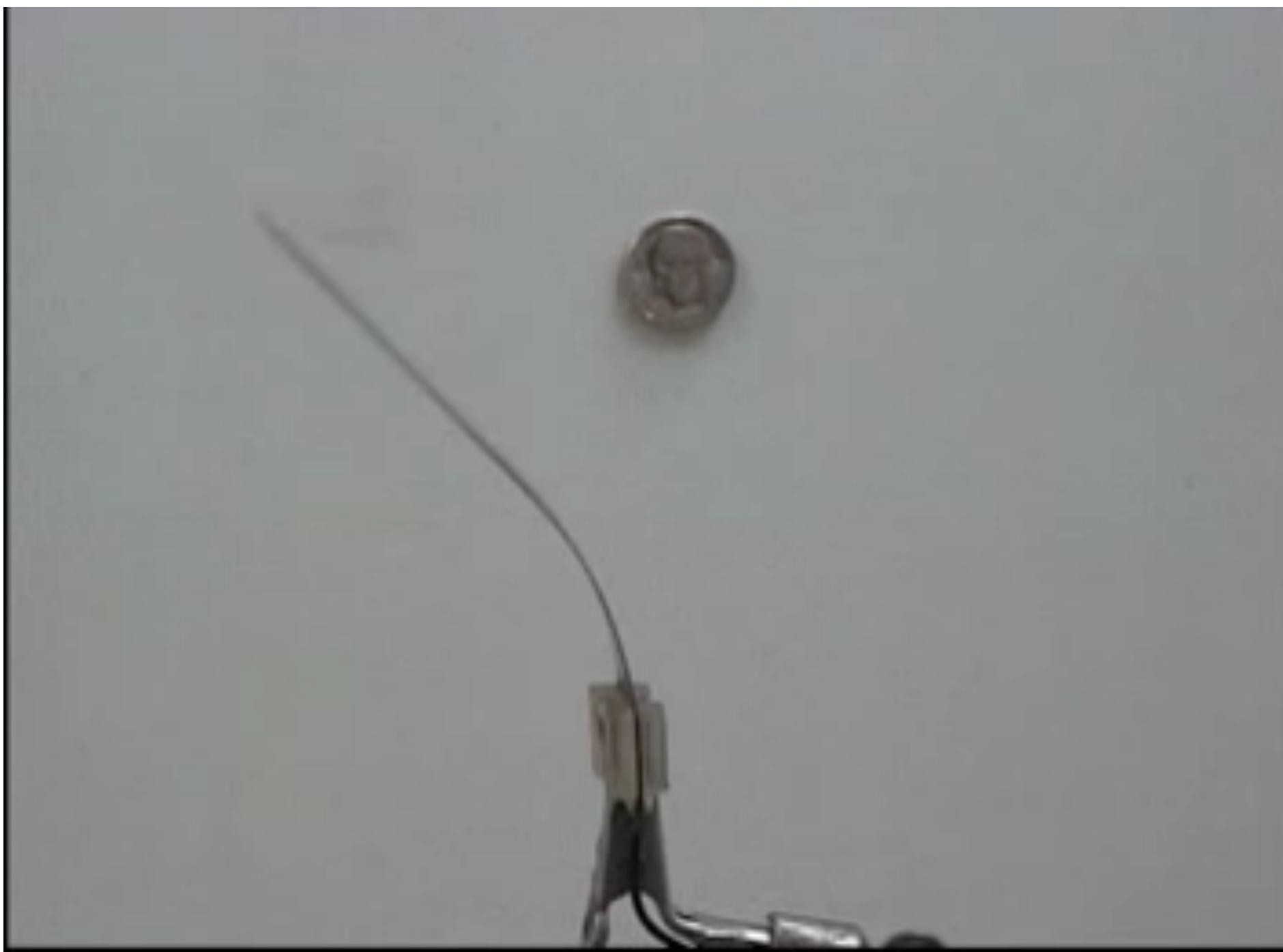
IPMC Actuators



IPMC Sensors



Macro-sized IPMC



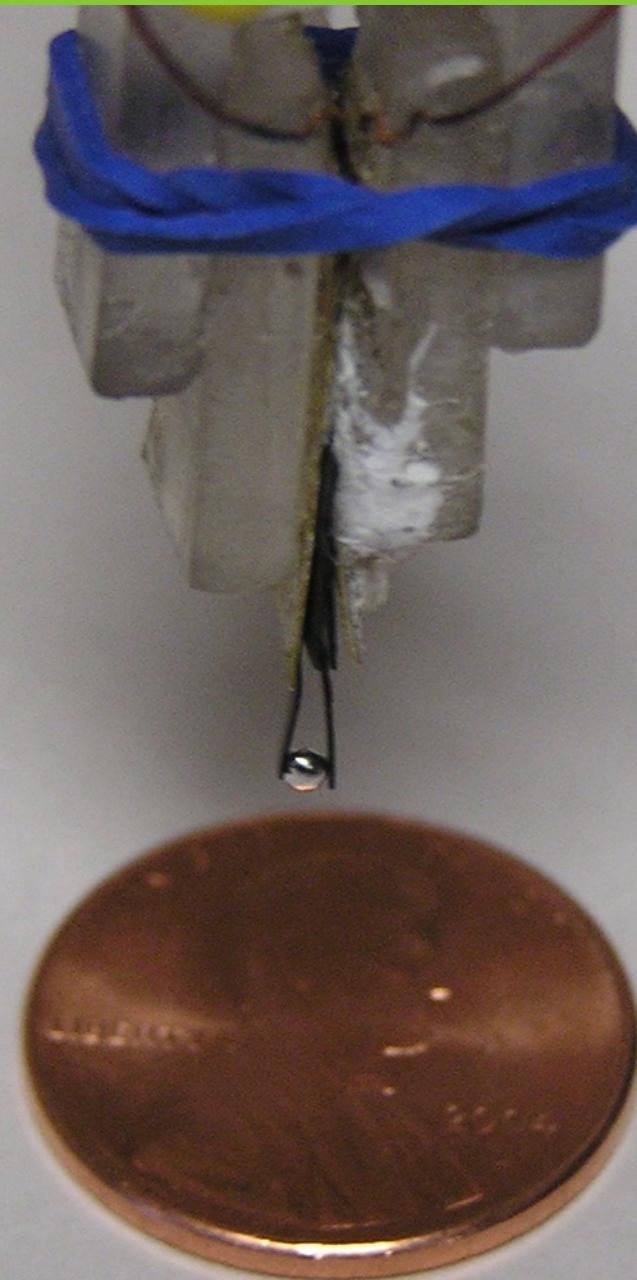
Resonance - Macro



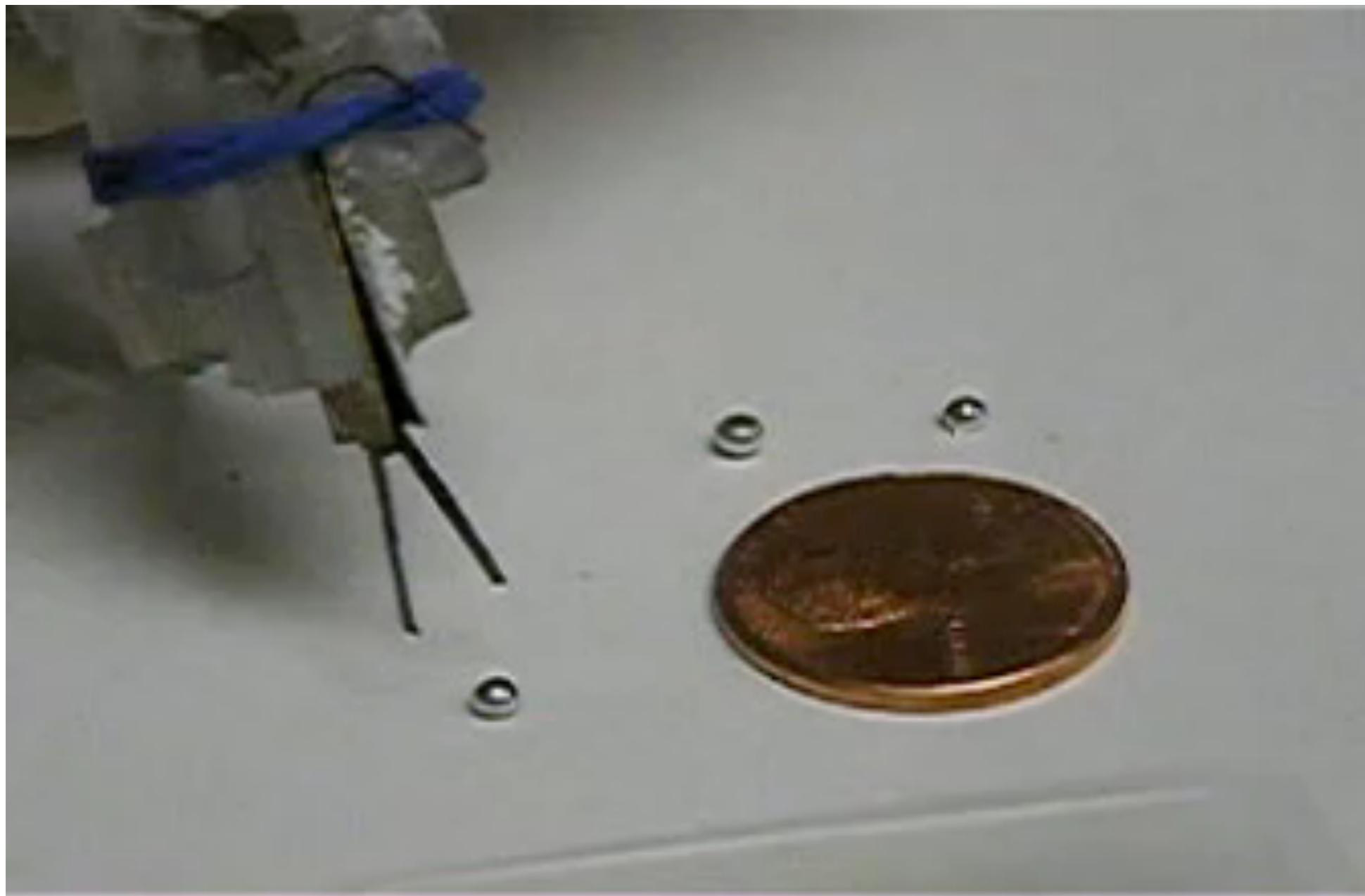
First Microgripper



Rigid Object Micromanipulation



Rigid Object Micromanipulation



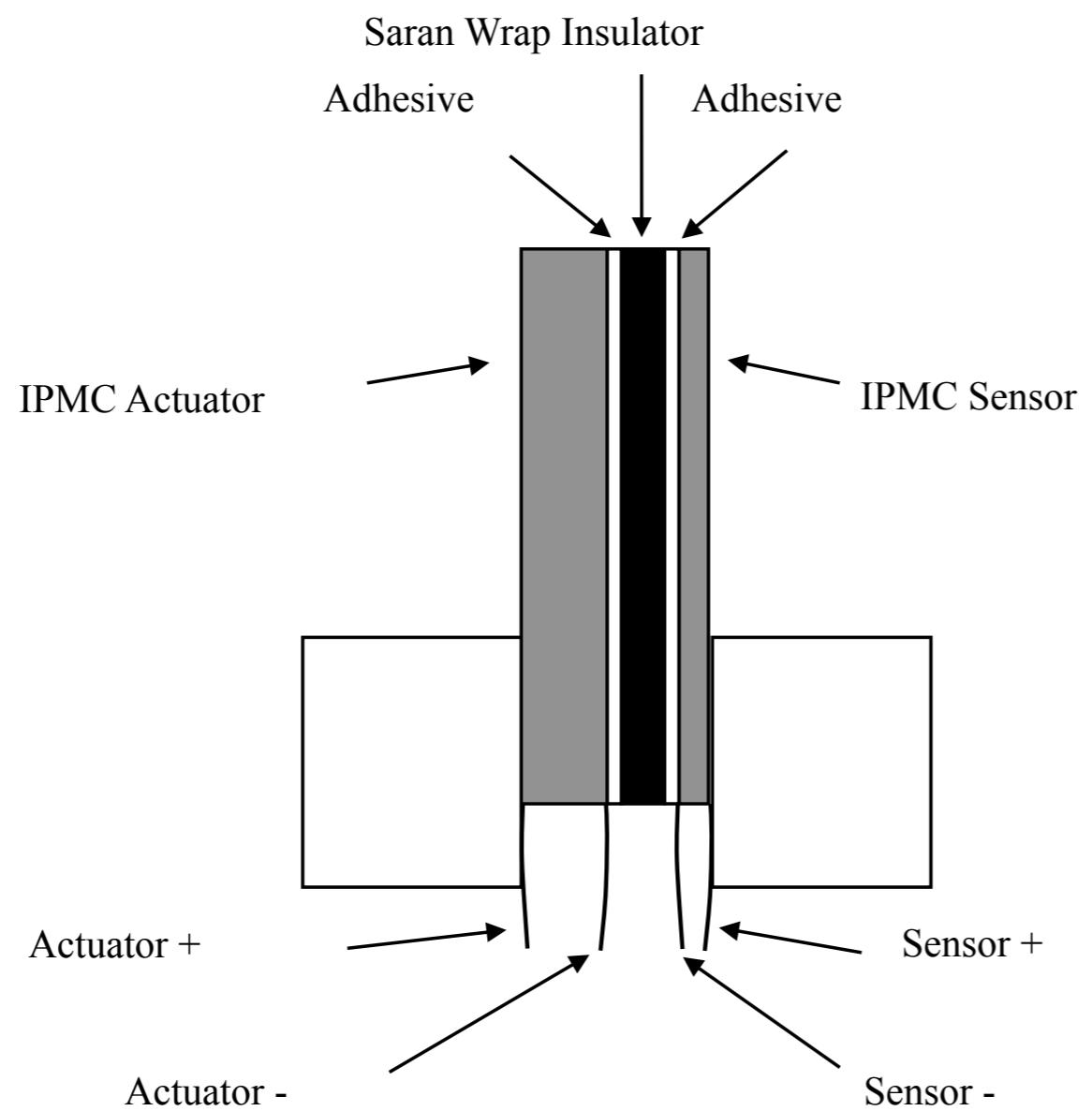
Flexible Object Micromanipulation

Yannick Gouin
Felix Ledergerber

IPMC Microgripper

- IPMC suited for microgrippers
 - IPMC sensor and actuator
 - IPMC weak
 - Gravity for small objects also weak
- IPMC suited to bio applications
 - Compliant - will not damage cells
 - Low voltage actuation
 - Work in dry or wet environments
 - Avoids hydrolysis in wet environments

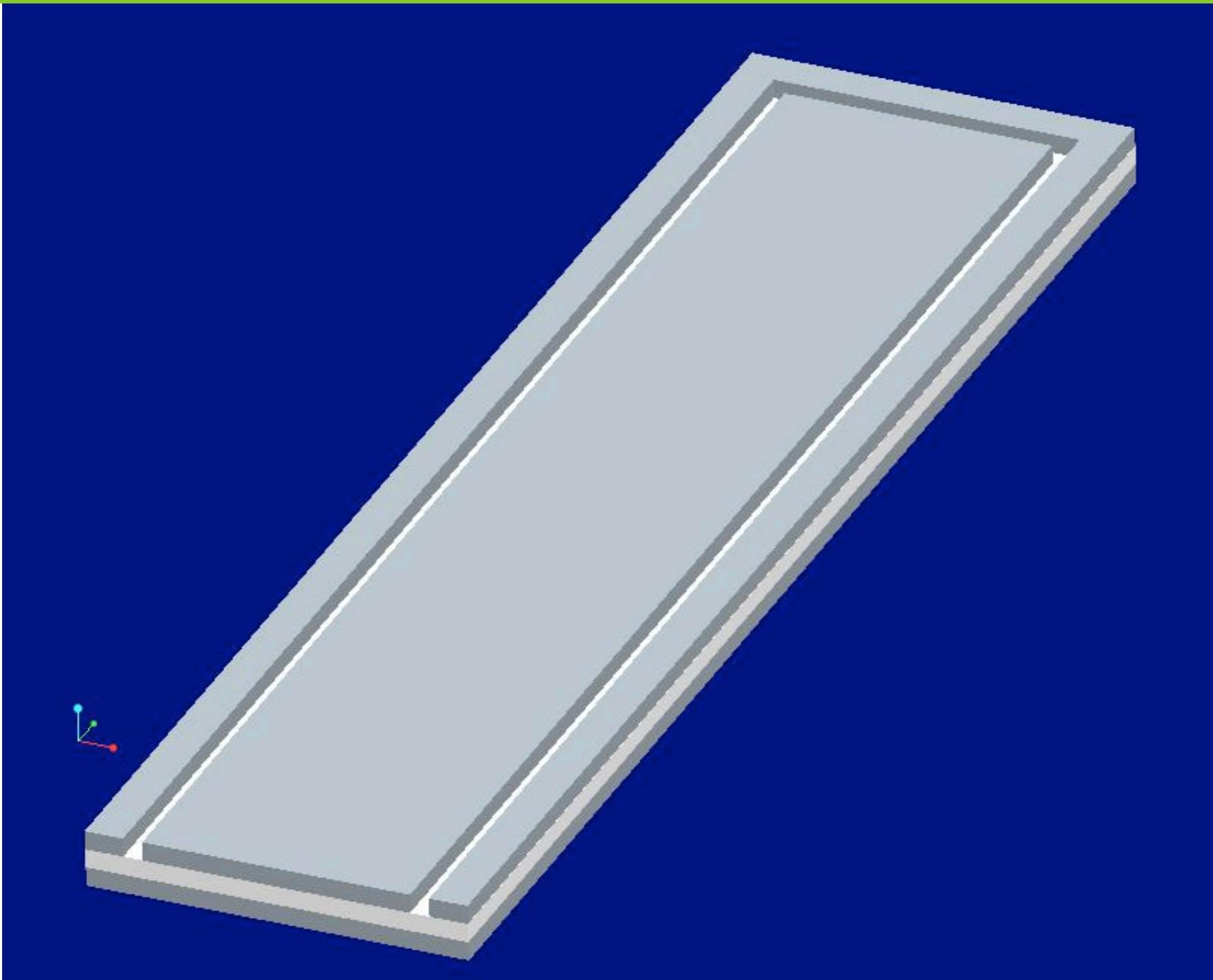
First Approach



Sensing Problem

- IPMC sensing using charge works well at macro-scale
- For microgrippers
 - Small area
 - Low charge
 - Low voltage - microvolts
 - Cannot extract signal from noise

New Approach to Sensing



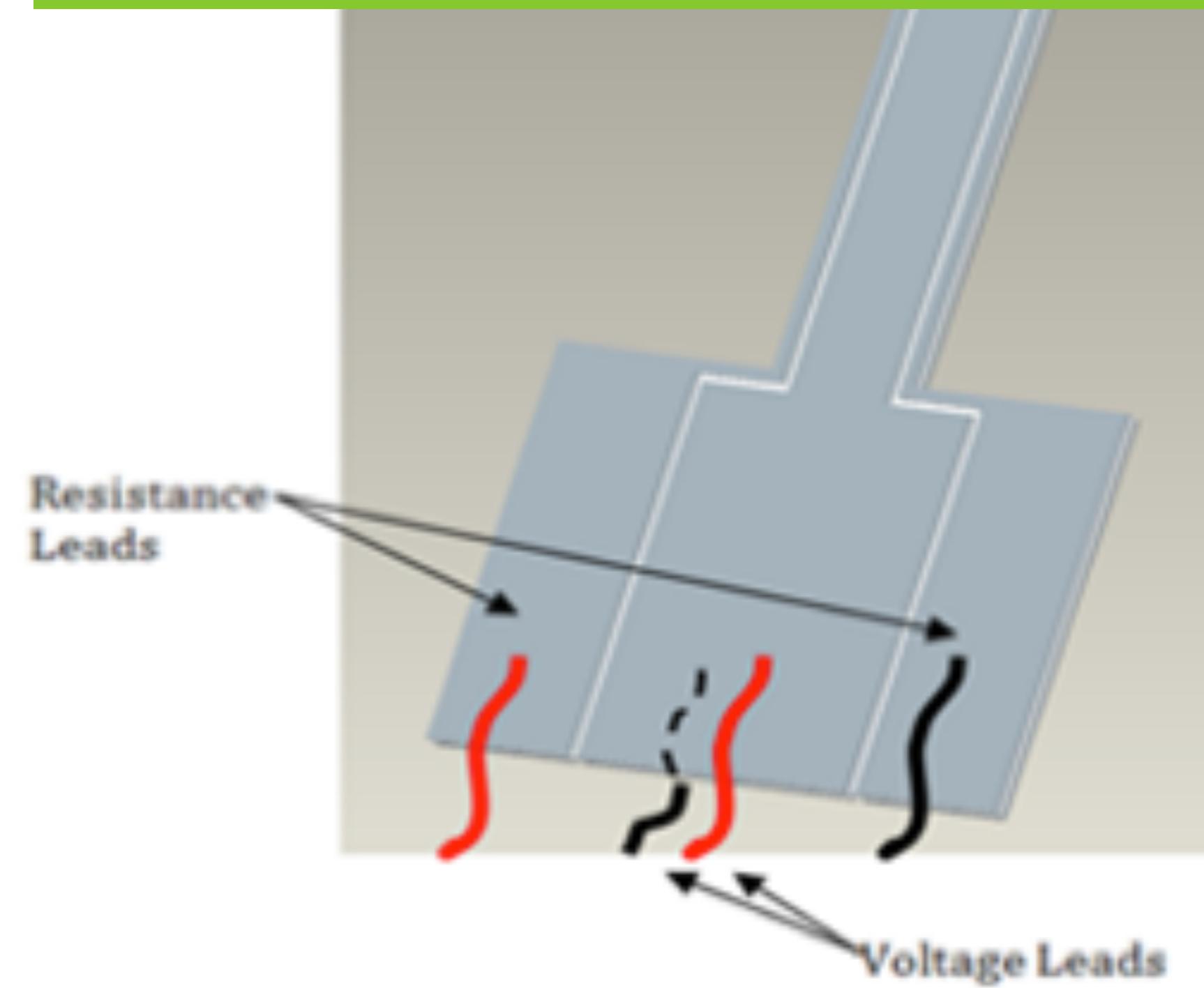
Cutting the Trench

Artificial Muscle
Laser Cutting Workstation

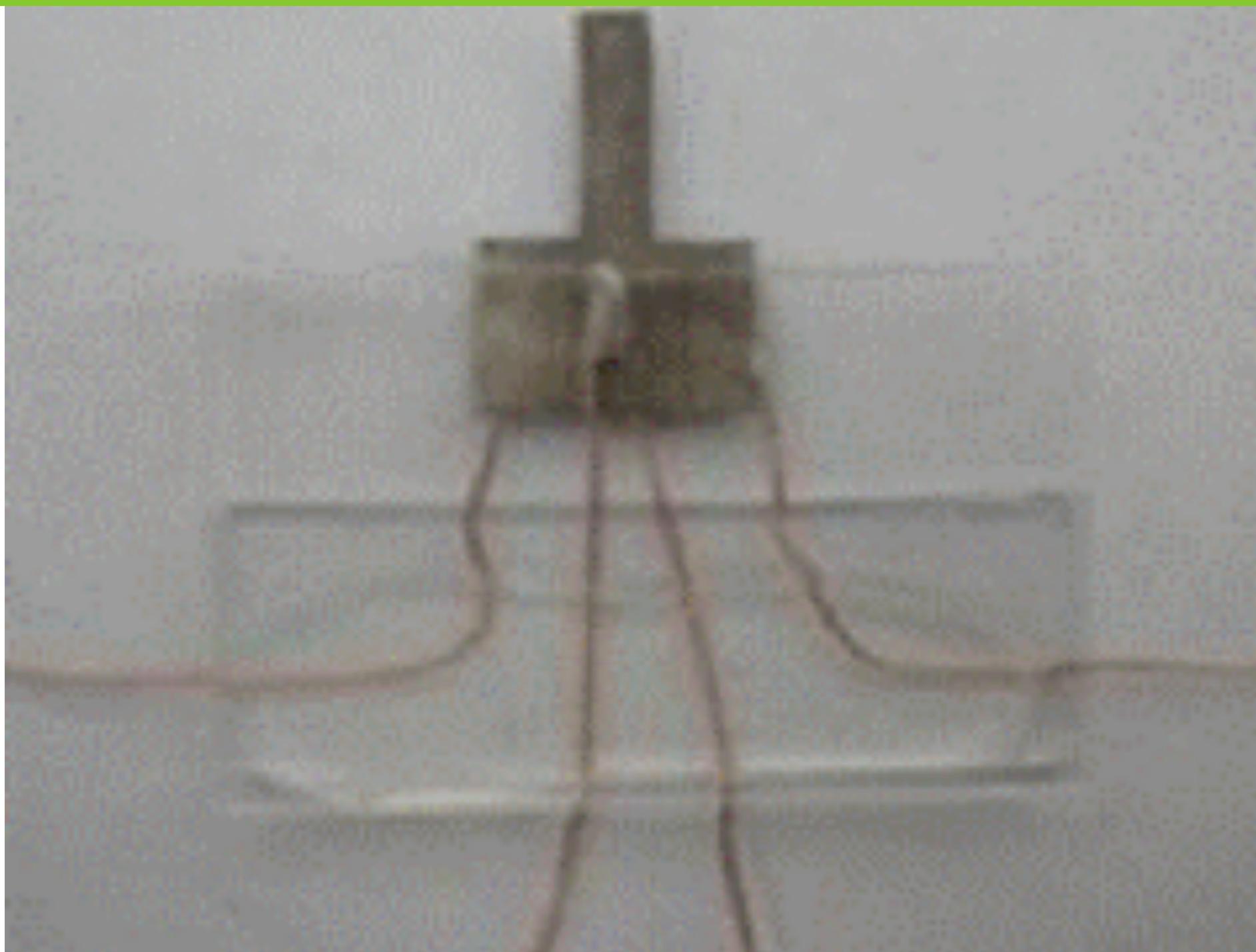
University of New Mexico

April 2008

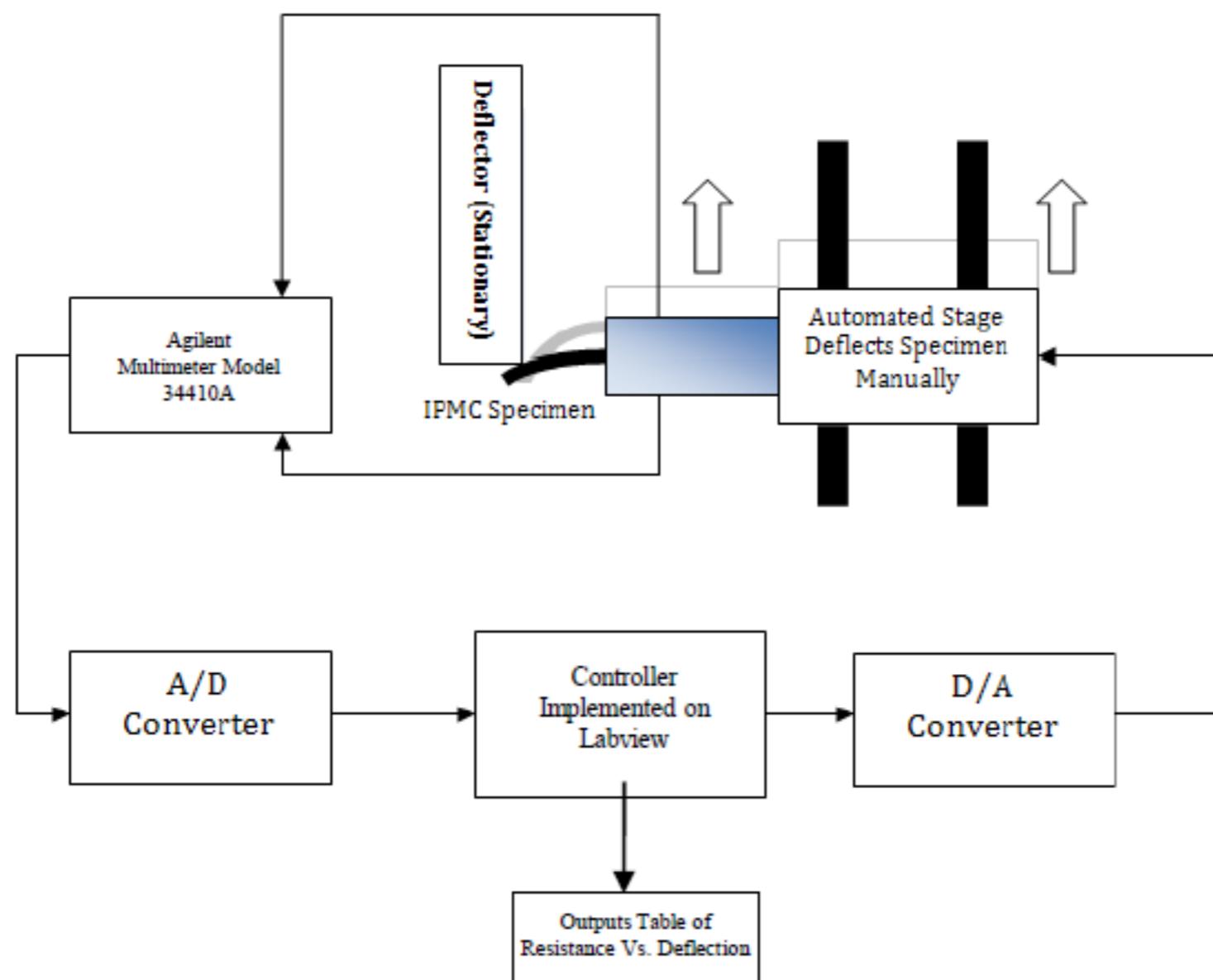
Proposed Finger



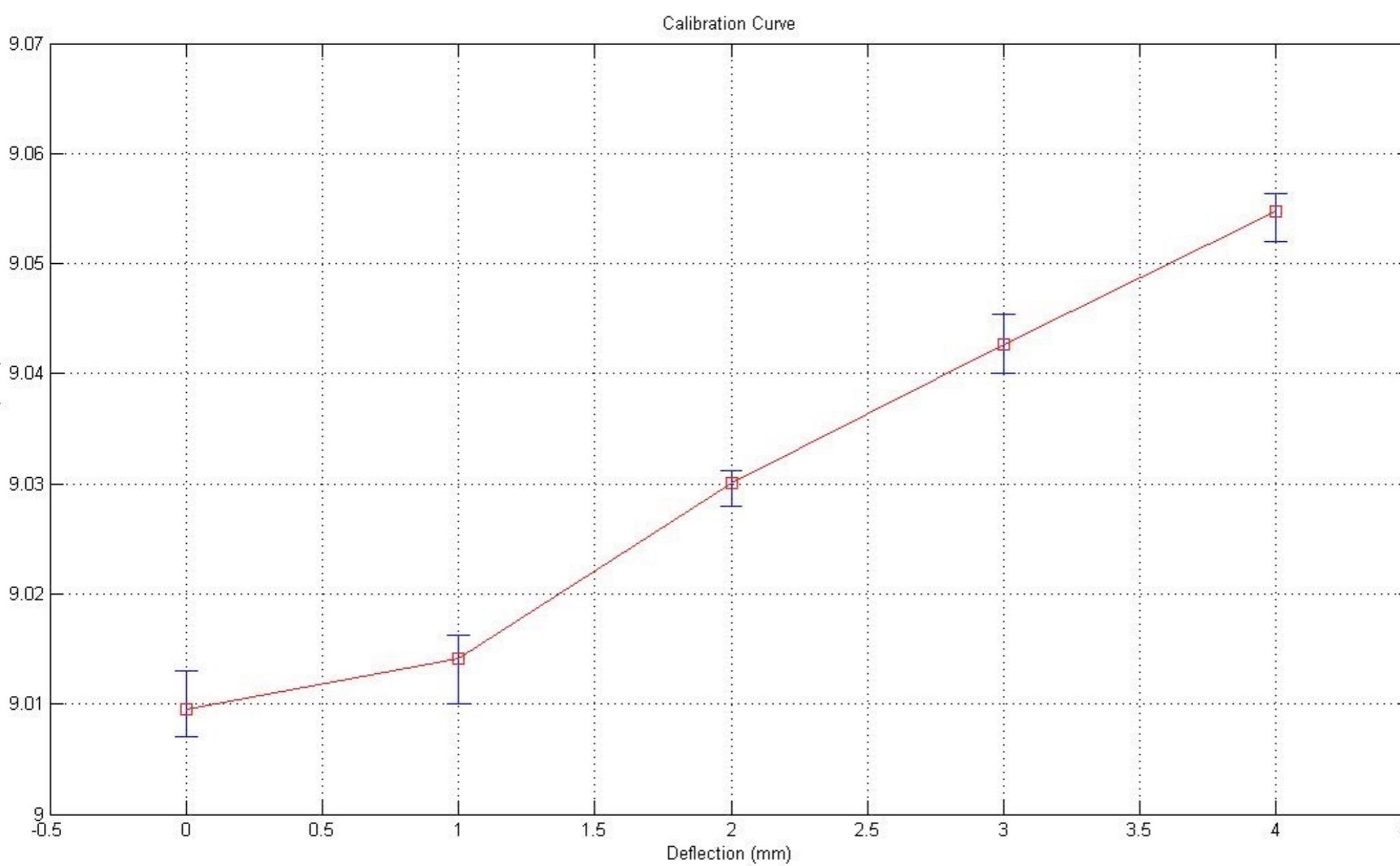
Experimental Results



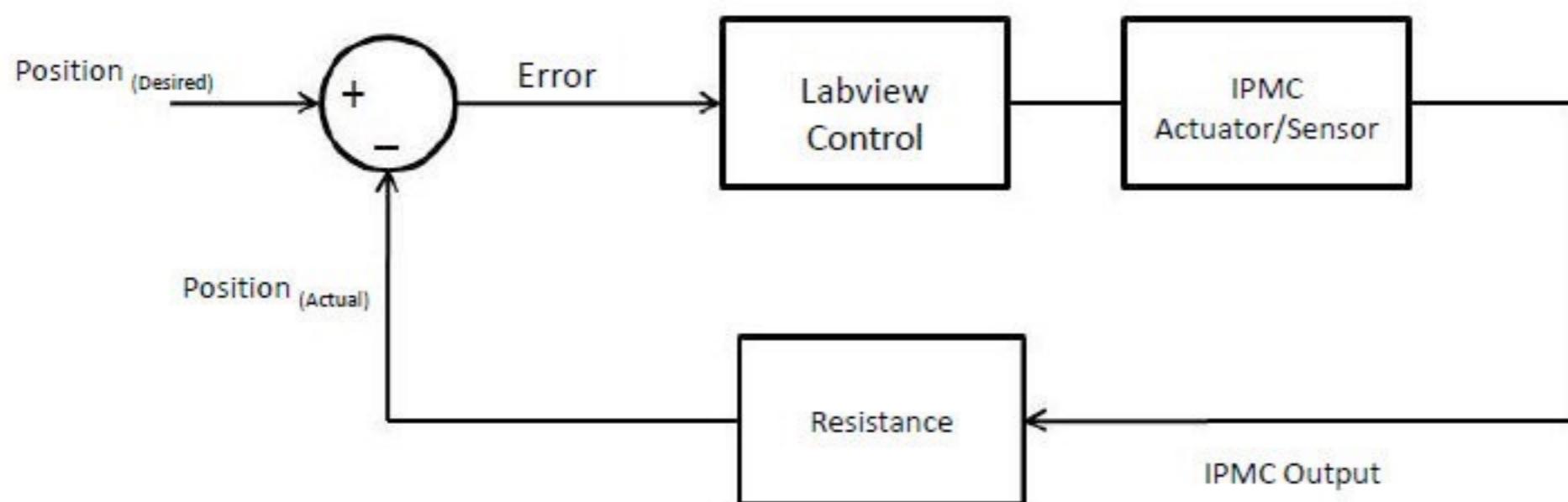
Lab Setup



Resistance vs. Deflection



Closed Loop Controller



Results

- Open loop control
 - 0.224 mm variation
- Close loop control
 - 0.050 mm variation
 - Most of variation is transient response

Closed Loop Pick and Place

IPMC Artificial Muscle Microgripper
Lifting Polymer Spheres

University of New Mexico 2011
Microgripper Lab

Applications

- Manipulation of flexible bio-objects
 - Suction pipette may damage cells
 - Oocytes and related bio-materials
- Manipulation of rigid objects
 - MEMS assembly

Conclusions

- Large scale robotics
 - Swing-free algorithm
 - Impedance control
 - Assembly
- Small scale robotics
 - IPMC microgripper
 - Cut trench to measure resistance to detect deflection
 - Closed loop controller for microgripper